

DC-10-30, N35084, 29 August 1997

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| Aircraft Type and Registration: | DC-10-30, N35084 |
| No & Type of Engines: | 3 General Electric CF6-50C2 turbofan engines |
| Year of Manufacture: | 1979 |
| Date & Time (UTC): | 29 August 1997 at approximately 1000 hrs |
| Location: | Near Knutsford service area, M6 Motorway |
| Type of Flight: | Public Transport |
| Persons on Board: | Crew - 14 - Passengers - 103 |
| Injuries: | Crew - None - Passengers - None |
| Nature of Damage: | Loss of right engine core cowl, damage to left cowl, exhaust nozzle and EGT sensing system |
| Commander's Licence: | Airline Transport Pilot's Licence |
| Commander's Age: | N/K |
| Commander's Flying Experience: | N/K |
| | Last 90 days - N/K |
| | Last 28 days - N/K |
| Information Source: | AAIB Field Investigation |

At approximately 1000 hrs, motorists on the M6 motorway just South of Junction 19 reported seeing sizeable pieces of metal falling from the sky and landing on, or near, the verges. No reports were received of any injury or damage caused on the ground. A police patrol was sent to investigate and gathered up about eight pieces of what was clearly aircraft debris, the largest piece being a stiffened sheet metal panel measuring roughly 4 feet x 2 feet. The police contacted Manchester Air Traffic Control (ATC) who, in turn, advised the AAIB Duty Co-ordinator.

ATC were asked for a list of aircraft which had used the particular Standard Instrument Departure route which would take the aircraft over the debris location and they replied that there had been two aircraft in the vicinity, one a Boeing 737 and the other a DC-10 on a scheduled flight to Newark, New Jersey. The pieces were despatched to AAIB and were quickly identified as comprising about 70% of a DC-10 engine right-hand core cowl (see Diagram).

The operator of the flight was contacted for information, and admitted that the aircraft in question, registration N35084, had indeed landed at Newark with the right-hand core cowl of No 3 engine missing. The flight crew were apparently unaware of the loss but had noted a loss of Exhaust Gas Temperature (EGT) indications shortly after take off. Although the FAA Operational Difficulty Report filed by the operator stated that both left and right cowls were missing on arrival, subsequent enquiries by AAIB produced a response that the left cowl had remained on the aircraft, in a badly damaged state. Other damage required replacement of the EGT strakes, lower vent system manifold and the exhaust nozzle.

Inspection of the parts held at the AAIB showed that only one of the three hinge fittings had remained on the cowl - the remainder having torn out of the cowl structure, as had the lower locking clasps. Both halves of the hinge were present, including the half normally fastened to the engine pylon using three steel bolts. The upper two of these bolts located in captive, self-aligning nuts retained within the hinge fitting and the remains of the bolt shanks were still in place (see photograph). The lower attachment was a more conventional nut-and-bolt arrangement, passing through a hole in the fitting. No parts of this bolt were present, but the distortion of the fitting at this location strongly suggested that the bolt had been fitted and had failed under overload forces.

This was not the case with the upper bolts and the clean, flat appearance of the fracture faces suggested that failure had occurred under fatigue conditions. The bolts were sent for metallurgical examination which confirmed that tension fatigue was present in both fractures. One bolt had fractured completely under medium-cycle fatigue loading whilst the other, failing later, also had an area of fast fracture. Hardness testing showed that the material strength of both bolts exceeded the minimum drawing requirements. When removed for this purpose, it was found that both bolts were 'threadbound' i.e. they had bottomed-out in the self-aligning captive nuts.

The two halves of the hinge fitting itself were made from Titanium. The half which was normally attached to the pylon had been quite extensively damaged apparently by contact with its corresponding half in the closed position. This damage was not reflected in the other half of the hinge, which only had minor witness marks and was probably not the original part which mated with the fixed half mounted on the pylon (see photograph 1). This latter half also had evidence of quite severe wear around one of the holes through which the fractured bolts had passed. One of the holes had been repaired by bushing but the other was unrepaired and was oversized and ovalised (see photograph 2). There was evidence of red primer paint on the hinge and the bolt shanks and, indeed, some of the paint had penetrated the fatigue crack in the bolt from the unbushed hole, indicating that the crack was present when paint was applied in the area. The bolt which had suffered 100% fatigue cracking had been in the bushed hole.

Maintenance History

The aircraft had been purchased by the current operator in 1997 when it was sent to a third party maintenance organisation in the USA for a 'C' check and customisation to their specification. This work was done in June 1997. At the time of the incident the aircraft had flown 70,584 hours and accumulated 14,995 landings. When approached for detail regarding significant work in the subject area, the operator could not provide any relevant history. The external appearance of the panel, which had a highly polished natural metal finish, suggested that the 'C' check had included at least some cosmetic work in the area.

Discussion

Information from Douglas Aircraft (Boeing) suggests that this is probably a unique occurrence. Although engine cowling losses are not unknown on virtually any make of engine/airframe, the usual reason is improper fastening or installation following maintenance. Fatigue failures of attachment hardware is less common and the reasons for it more complex unless it is simply accepted that components have reached the end of their fatigue life, in which case similar reports might be expected from other, higher time, aircraft.

There were no metallurgical reasons for the fatigue of the hinge attachment bolts. The material exceeded the minimum strength required and the dimensions and manufacturing processes (as far as could be determined) appeared correct. However, it is significant that the first bolt to develop fatigue was associated with the repaired, bushed hole. Clearly this was the one which was taking the majority of the load, presumably because of the clearance which had opened-up as the other hole fretted. It is logical to presume that, at the time the bushed repair was done, the other hole was not judged sufficiently worn to justify such action, although the wear present at the time of the incident was fairly gross, as can be seen from the photograph. When the first bolt failed in fatigue, all the load transferred to the unbushed bolt which started to fatigue before failing in overload.

The effect of both bolts being threadbound is difficult to quantify as is the reason. Because the other halves of the fractured bolts were not recovered, a check on their total length was not possible. It is possible that washers had been omitted on assembly but, again, this could not be verified. The fitting itself did not show signs of significant fretting on its inboard face which might have suggested that there was insufficient clamping force between it and the pylon. It was suspected that the bruising damage to the hinge fitting shown in photograph 1 might have been caused by a previous cowl attachment problem but no records were available to confirm this and, in any case, metallurgical examination of the fractured pins did not suggest that a single overload event had initiated fatigue.

The operator was approached for information regarding the condition of the left side forward hinge attachment bolts. Unfortunately they replied that this fitting had also been replaced but the parts were not examined in detail and were discarded at Newark.

Subsequent Actions

Boeing have advised that they propose to revise their Maintenance Manual such that if any damage, such as bolt hole damage, elongation, loose bolts etc., is noted in the area, then bolt replacement will be required. Additionally, rebushing of the holes in the fitting will again require fitting of new bolts. They also intend to revise the Maintenance Planning Document to include a regular inspection of the area at 'C' check intervals (roughly every 12 to 24 months).