

# **Boeing 757-2T7, G-MONE**

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## **INCIDENT**

Aircraft Type and Registration:	Boeing 757-2T7, G-MONE
No & Type of Engines:	2 Rolls-Royce RB211-535E4 turbofan engines
Year of Manufacture:	1985
Date & Time (UTC):	22 January 2000 at 1200 hrs
Location:	London Gatwick Airport
Type of Flight:	Public Transport
Persons on Board:	Crew 10 - Passengers - 74
Injuries:	Crew None - Passengers - None
Nature of Damage:	Failed nose landing gear retract actuator and failed lock actuator. Bent lock links and other components in nose landing gear area. Damaged landing gear position sensors
Commander's Licence:	Airline Transport Pilots Licence
Commander's Age:	59 years
Commander's Flying Experience:	16,358 hours (of which 9,942 were on type) Last 90 days - 118 hours  Last 28 days - 25 hours
Information Source:	Aircraft Accident Report Form submitted by the pilot, metallurgical examination of failed component

## **Background**

The Captain reported the following events. On take off from Salzburg (SZG) a loud bang was heard from the area just below the front of the aircraft. As no other indications were present it was presumed to be the result of a birdstrike. On approach to Gatwick, however, on selecting landing gear down, a very loud bang was heard and the aircraft shook. The nose landing gear indicated unlocked amber. A go-around was therefore carried out.

During this manoeuvre, tower observers noted that the landing gear appeared to be down whilst the crew of a taxiing aircraft considered that it was down but not locked. A PAN call was transmitted and the QRH drill carried out. The nose landing gear amber warning remained.

The senior cabin crew member was given a Nature Intention Time Security (NITS) brief and the passengers were briefed by the cabin crew and kept informed of the situation by the Captain. A precautionary landing was then carried out with emergency services in attendance. The nose landing gear remained in the down and locked position. The aircraft was taxied clear of the runway and an inspection was requested. Ground-locks were put in and the aircraft was taxied onto the stand without further incident.

Closer examination of the aircraft revealed that the nose landing gear retract actuator eye-end had failed at the junction of the eye and its threaded section (*see Fig 1*). The nose landing gear lock actuator had also failed and various mechanical components of the nose landing gear were bent.

The failed items were supplied to the AAIB who arranged a metallurgical examination of the fracture surfaces. This showed that the lock actuator had failed as a result of ductile overload, whilst the nose landing gear retract actuator had suffered a fatigue failure.

### **Component description**

The retract actuator eye-end is screwed into the end of the actuator piston rod. It is locked in position by a cupped collar positioned between the eye-end and the rod. The collar is clamped against the end of the rod by means of a shoulder on the body of the eye end, positioned where the eye-end profile merges into the plain cylindrical portion on which the attachment thread is formed. (see Fig 1).

The locking collar is positioned with the cup facing the eye bolt and located rotationally relative to the piston rod by means of a locating tag engaging in a slot machined into the rod. The cupped sides of the collar are then peened into two recesses in the body of the eye-end after component assembly, thus locking the eye-end relative to the piston rod. The failure was orientated in the plane of the collar and the shoulder.

### **Detailed examination**

The fatigue failure exhibited a large number of closely spaced striations where they could be distinguished, although, over much of the section, individual striations were not clearly identifiable. The machined face of the shoulder beneath the lock collar had been almost entirely obliterated by a series of deep marks created by either a saw or a file. The fatigue crack clearly had origins associated with some of the above pre-existing damage and had extended to a point approximately one third of the way across the cylindrical section. Examination of the face of the collar in contact with the shoulder, revealed a pattern of witness marks matching in mirror image the saw or file marks on the latter. (See Figs 2&3).

### **Component history**

The aircraft operator reported that there was no record of the actuator having been removed from the aircraft or worked upon since the work associated with a Service Bulletin (SB) had been carried out on the corresponding retract actuators of 3 Boeing 757 aircraft on the fleet, including G-MONE, in 1988. This had required the units to be removed from the aircraft and routed to the operating company's hydraulic bay for dismantling. Examination of the other two affected actuators has

revealed that one had similar mechanical damage to the shoulder of the eye-end under the locking collar. On both actuators the eye ends were not torque tightened to the correct value.

A further examination of the records indicated that the two personnel employed in the hydraulic bay at the time the SB was carried out, one of whom certified the work, left the company soon after, in 1989. The bay supervisor at the time left the Company in 1990. It is not thought that these individuals are still employed in aviation.

## **Discussion**

The evidence makes it clear that the fatigue cracking originated from the stress-raisers created by the mechanical damage seen adjacent to the shoulder. Although the number of striations on the fracture faces could not be counted, there was clearly a very large number, representing a large number of load cycles having taken place between crack initiation and failure. (It is thought that one cycle of high loading occurs during landing gear retraction and lesser loading during extension).

The mechanical damage was clearly present when the actuator was last reassembled, the eye-end having been screwed into position onto a new locking collar creating the mirror image tool marks visible thereon. (A new collar must have been used, since the old collar could not have been removed to unlock the two components without inflicting damage which would have remained evident on the collar. No such damage was present.) The mechanical damage is presumed to have been inflicted whilst the eye-end was disassembled from the piston rod or during the previous disassembly process.

The similarity between the mechanical damage to the shoulder and that observed on one of the other retract actuators changed on the fleet at the same time leaves little doubt that all the corresponding damage was inflicted at that same time. It seems likely that this was done in an attempt to free the locking collars previously installed. It is understood that the collar area is normally coated in sealant so the means by which it is secured (ie the peening and the locking tag) are not visible.

Disassembly of the eye-end from the piston rod requires the sealant to be removed first in order for the peened area and/or the tang to be located. Should the operative not have established the details of the locking method, and not removed the sealant, it would not have been possible to remove the lock collar and free the eye-end from the rod without destroying the collar. In so doing, it is very probable that damage would be inflicted to the machined face of the shoulder and the adjacent cylindrical section of the eye-end.

The lock actuator failure was a ductile fracture typical of overload. Since a bang was heard during retraction, and the highest loading on the retract actuator appears to occur at or near the end of the retract cycle, it can reasonably be assumed that its failure occurred after take off from SZG. It

is difficult, however, to visualise a mechanism by which the lock actuator could have been damaged during retraction as a result of the retract actuator failure. As no landing gear indications were present in the cruise, it is probable that the up-lock was engaged and its actuator still intact during this period.

To lower the landing gear would normally require the up-lock to release. The doors would also need to open and the retract actuator to extend. With a failed retract actuator, however, once the up-lock actuator had released the geometric up-lock, the normal damping would have been absent leaving nothing other than the doors to prevent the leg from descending under its own weight.

Once the doors were open, the leg would have been free to fall unrestrained to the fully down position. It is likely that the rapid, unrestrained descent of the leg, coupled with the effect of the two locksprings, caused much more rapid extension of the lock actuator ram than could be achieved by normal hydraulic action. Alternatively elastic and plastic deformation of the structure and components of the leg mechanism may have resulted in over-travel of the lock actuator ram. Either way, a mechanism appears to exist for applying tensile overload to the small diameter ramrod of the lock actuator, which would account for its tensile failure. This undamped descent of the leg probably also accounts for the bend damage to various other components of the landing gear mechanism.

Although the lock actuator was thereafter not capable of ensuring that the down-lock remained made, the two locksprings performed that function.

## Conclusions

The incident was caused by failure of the eye-end of the nose landing gear retract actuator. This failure resulted from long-term fatigue crack, which had propagated from an area of mechanical damage inflicted by means of a saw or file. The damage had occurred when the actuator was last dismantled, 11 years before the incident, as a result of the use of inappropriate workshop practices during dismantling of the component. The actuator was then re-assembled with the damage still present. The operators quality system in place at that time failed to detect the use of unsatisfactory workshop procedures.